

## Quiz 12 Chemical Engineering Thermodynamics April 11, 2019

An absorption refrigerator\* uses a refrigerant and an absorber rather than a refrigerant/compressor in a normal refrigerator. It runs off a low-level heat source such as solar heat or a gas burner (RV refrigerators). In the ammonia (1) and water (2) refrigerator, water is the absorber, and ammonia is the refrigerant. In one iteration of such a refrigerator, ammonia vapor is absorbed into water at 40.6°C and 0.515 MPa,  $x_1 = 0.5$  ammonia (*Absorber*).

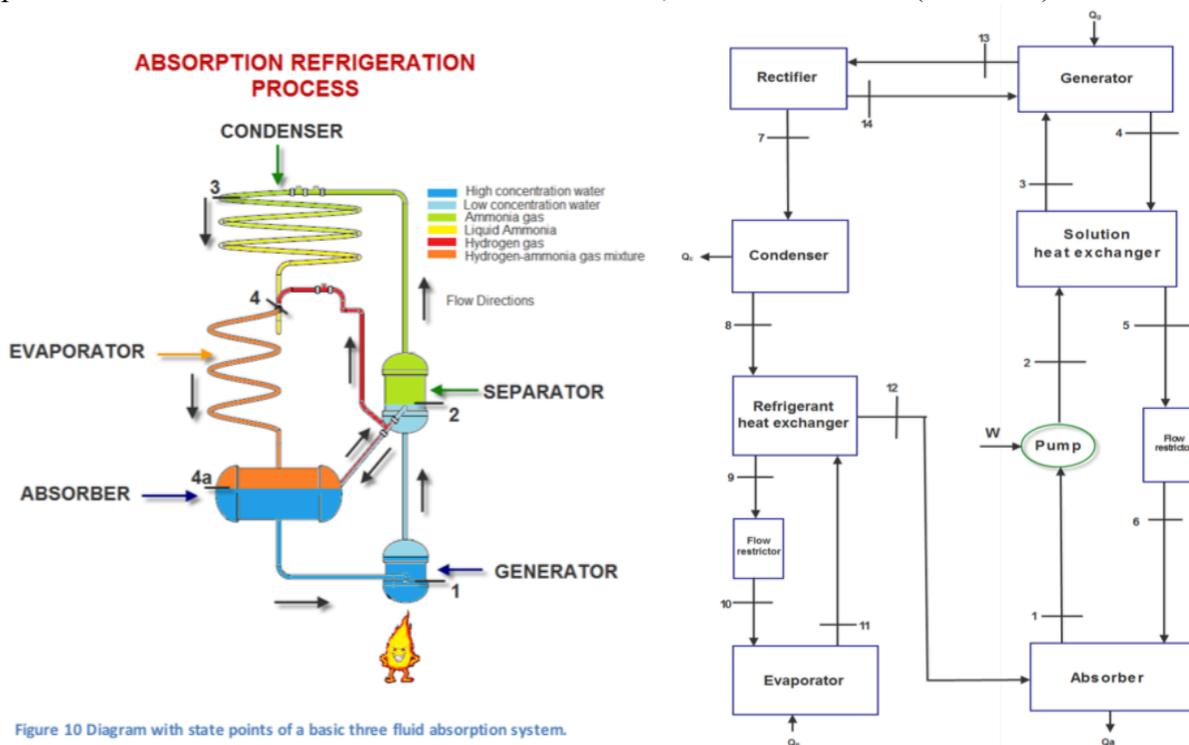


Figure 10 Diagram with state points of a basic three fluid absorption system.

**USE THE ANSWER SHEET TO GIVE YOUR ANSWERS  
BUT ALSO SHOW WORK (show some work if you use Excel).**

- Ganesh\*\* reports an equilibrium point of  $P=3.5$  MPa,  $T = 90^\circ\text{C}$ ,  $x_1=0.709$  and  $y_1 = 0.871$  for the ammonia/water system. Use these values to calculate the **two**-parameter Margules coefficients,  $A_{12}$  and  $A_{21}$ .
- Calculate the **one**-parameter Margules coefficient " $A_{12}$ " using " $A_{12}$ " =  $(x_1 \ln \gamma_1 + x_2 \ln \gamma_2)/(x_1 x_2)$ .
- Compare** " $A_{12}$ " from part "b" with the two-parameter result and comment on the advantage of the two-component model using the Redlich-Kister form,  $G_E/RT = x_1 x_2 (B_{12} + C_{12} (x_1 - x_2))$  considering  $B_{12} = (A_{21} + A_{12})/2$  and  $C_{12} = (A_{21} - A_{12})/2$ . *That is, compare  $B_{12}$  with " $A_{12}$ " from the one-component model; and compare the value of  $C_{12}$  to  $B_{12}$  to assess the importance of asymmetry in  $G_E$  as a function of  $x_1$ .*
- Using the one-parameter Margules coefficient from part "b" calculate the bubble pressure in the absorber at 40.6°C and 0.515 MPa,  $x_1 = 0.5$ .
- Using the one-parameter Margules coefficient from part "b" calculate the dew pressure in the generator which is at 79.15°C,  $y_1 = 0.987$ . Proceed until reasonable convergence.

- f) Extra credit: The ammonia-water refrigerator had a small impact in the 1920's before widespread electrification in the US (Crosley Icyball manufactured in Cincinnati <https://en.wikipedia.org/wiki/Icyball> ) but it has had almost no impact in the developing world despite widespread need for refrigeration for vaccines and other uses. List some reasons that you think could explain why this absorption refrigerator hasn't found wider application in areas without electrification (Crosley delivered 10,000 Icyballs to Tanzania in the 1930's).

\* [https://web.wpi.edu/Pubs/E-project/Available/E-project-042612-110655/unrestricted/MQP-Design\\_and\\_Analysis\\_of\\_an\\_Absorption\\_Refrigeration\\_System.pdf](https://web.wpi.edu/Pubs/E-project/Available/E-project-042612-110655/unrestricted/MQP-Design_and_Analysis_of_an_Absorption_Refrigeration_System.pdf)

\*\* <http://shodhganga.inflibnet.ac.in/handle/10603/37842>

$$R = 8.314 \text{ J/(mole } ^\circ\text{K)}$$

$$\frac{G^E}{RT} = A_{12}x_1x_2 = x_1 \ln \gamma_1 + x_2 \ln \gamma_2$$

$$\ln \gamma_1 = A_{12}x_2^2$$

$$\ln \gamma_2 = A_{12}x_1^2$$

#### Antoine Constants (*T in °K P in Bar*)

|             | A    | B    | C     | T <sub>Min</sub> (°K) | T <sub>Max</sub> (°K) |
|-------------|------|------|-------|-----------------------|-----------------------|
| (1) Ammonia | 4.87 | 1110 | -10.4 | 240                   | 372                   |
| (2) Water   | 3.56 | 644  | -198  | 379                   | 573                   |
| (2) Water   | 4.65 | 1440 | -64.8 | 256                   | 373                   |

*T is in °K and P is in Bar*

$$\log_{10}(P) = A - (B / (T + C))$$

$$\frac{G^E}{RT} = x_1x_2(A_{21}x_1 + A_{12}x_2)$$

$$A_{12} = \left(2 - \frac{1}{x_2}\right) \frac{\ln \gamma_1}{x_2} + \frac{2 \ln \gamma_2}{x_1}$$

$$A_{21} = \left(2 - \frac{1}{x_1}\right) \frac{\ln \gamma_2}{x_1} + \frac{2 \ln \gamma_1}{x_2}$$

Modified Raoult's law.

$$y_i P = x_i \gamma_i P_i^{sat}$$

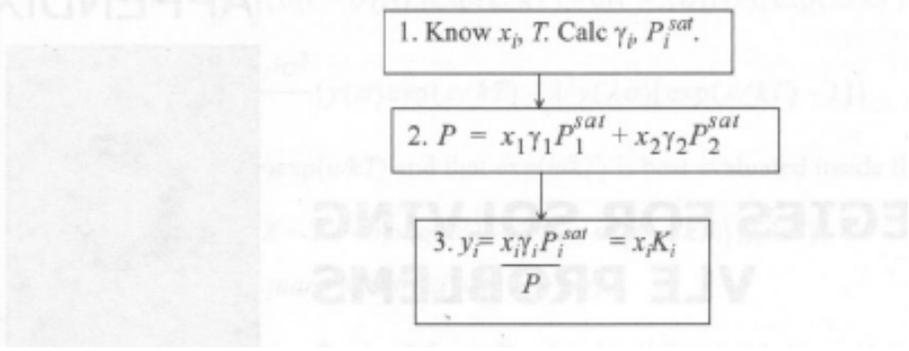
or

$$K_i = \frac{P_i^{sat}}{P}$$

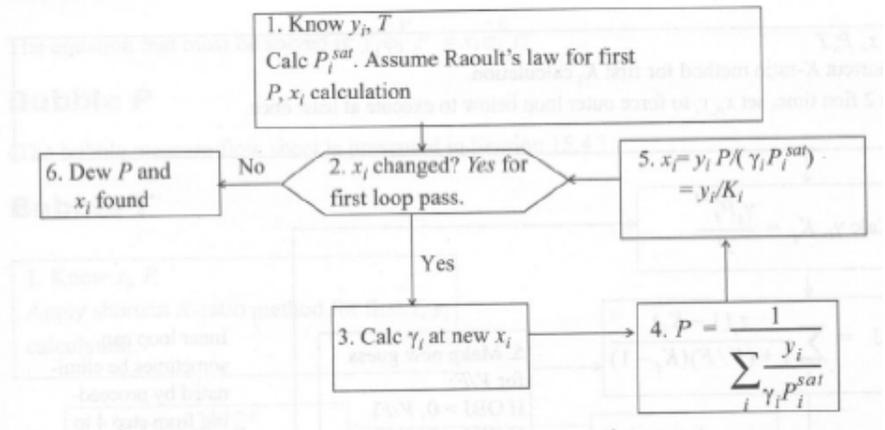
11.18

The equation that must be solved is:  $y_i P = x_i \gamma_i P_i^{sat}$

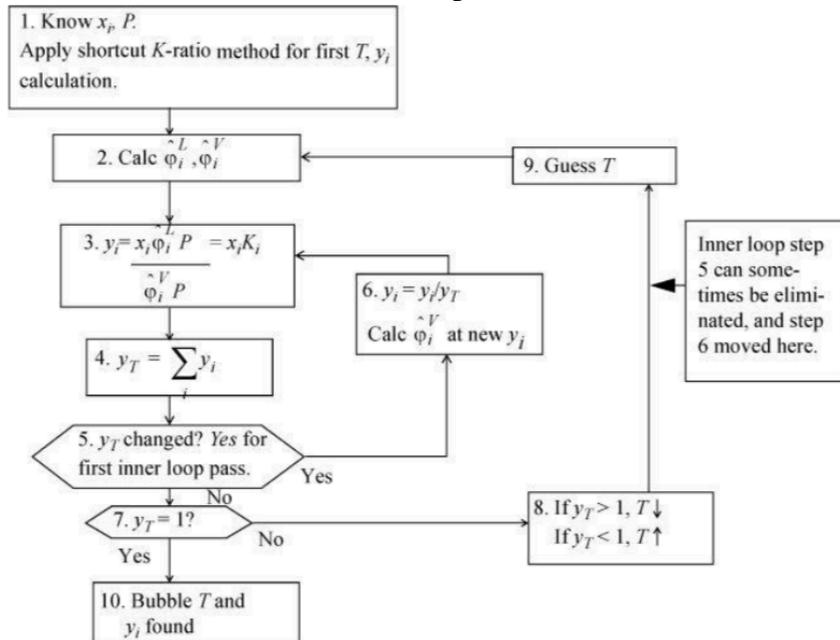
### Bubble P



### Dew P



### Bubble Temperature



## Answer Sheet

a)  $A_{12}$ :

$A_{21}$ :

b) " $A_{12}$ ":

c)  $B_{12}$ :

$C_{12}$ :

Compare  $B_{12}$  to " $A_{12}$ ":

Compare  $C_{12}$  to  $B_{12}$ :

d) Bubble Pressure:

e) Dew Pressure:

f) List some reasons:

## Answer Sheet

a)  $A_{12}$ : 9.90

$A_{21}$ : 1.22

b) " $A_{12}$ ": 3.75

c)  $B_{12}$ : 5.56

$C_{12}$ : -4.34

Compare  $B_{12}$  to " $A_{12}$ ":

This comparison reflects the difference in value at  $x = 0.5$ . The value is about 33% different so this is significant. It indicates that the one parameter model is not very good for this system in terms of the general value of  $A_{12}$ .

Compare  $C_{12}$  to  $B_{12}$ :

$C_{12}/B_{12}$  is about 32% which indicates a large degree of skewedness. The negative sign indicates that the curve is skewed to the left. This also indicates that the one parameter Margulus function is not very good for this system.

d) Bubble Pressure: 20.7 bar

e) Dew Pressure: 33.0 bar

f) List some reasons:

-Ammonia danger

-Comparison of cost with a solar panel and a conventional refrigerator. The corrosive nature of ammonia and the pressure of the system requires the use of stainless steel which is very expensive compared to a solar panel and a conventional refrigerator.

-Overall the system is "clunky".

-There is something like a street appeal to this kind of appliance and the ammonia refrigerator doesn't have street appeal. There might be a way to improve on this with careful design. Ammonia absorption refrigeration is widely used on the industrial scale, especially in the food processing industry.

-There are probably many more reasons.

|               |                           | TC         | TK         | P bar          |            |            |
|---------------|---------------------------|------------|------------|----------------|------------|------------|
|               |                           | 90         | 363        | 35             |            |            |
|               |                           | A          | B          | C              | D          |            |
| 1             | Ammonia                   | 4.87       | 1110       | -10.4          |            | Part a     |
| 2             | Water                     | 4.65       | 1440       | -64.8          |            | two param. |
|               |                           | Psat Bar   | x          | y              | gamma      | A (12;21)  |
| 1             | Ammonia                   | 52.7177531 | 0.709      | 0.871          | 0.815611   | 9.90       |
| 2             | Water                     | 0.66225639 | 0.291      | 0.129          | 23.4281831 | 1.22       |
| <b>Part b</b> | A12 one parameter<br>3.75 |            |            |                |            |            |
| <b>Part c</b> | B12                       | C12        | C12(x1-x2) | C12(x1-x2)/B12 |            |            |
|               |                           | 5.56       | -4.34      | -1.8143553     | -0.326183  |            |
|               | Value at x=.5             |            |            | Skewedness     |            |            |
|               |                           |            |            |                |            |            |
|               |                           | TC         | TK         | P bar          |            |            |
|               |                           | 40.6       | 313.6      |                |            |            |
|               |                           | A          | B          | C              |            |            |
| 1             | Ammonia                   | 4.87       | 1110       | -10.4          |            |            |
| 2             | Water                     | 4.65       | 1440       | -64.8          |            | Part d     |
|               |                           | Psat Bar   | x          | y              | gamma      | P bar      |
| 1             | Ammonia                   | 16.1826683 | 0.5        | 0.99552061     | 2.5523317  | 20.7       |
| 2             | Water                     | 0.07281463 | 0.5        | 0.00447939     | 2.5523317  |            |

| Psat1 bar  | Psat2 bar  |            |            |            |        |
|------------|------------|------------|------------|------------|--------|
| 42.01813   | 0.437829   |            |            |            |        |
|            |            | g1         | g2         | P bar      |        |
| x1         | x2         | 1          | 1          | 18.8       |        |
| 0.44160937 | 0.5582088  | 3.21712784 | 2.07782285 | 46.3146565 |        |
| 0.33816648 | 0.66183352 | 5.16853103 | 1.53547095 | 41.8722831 |        |
| 0.19030051 | 0.80969949 | 11.687849  | 1.14545686 | 35.8021733 |        |
| 0.07195405 | 0.92804595 | 25.2735864 | 1.01960489 | 33.2773545 |        |
| 0.03092875 | 0.96907125 | 33.8392573 | 1.00359364 | 33.0253203 |        |
| 0.02292486 | 0.97707514 | 35.8747741 | 1.00197275 | 33.0160801 |        |
| 0.02161806 | 0.97838194 | 36.2202031 | 1.00175406 | 33.0158352 | Part e |
| 0.02141173 | 0.97858827 | 36.2750881 | 1.00172071 | 33.0158291 |        |
| 0.02137933 | 0.97862067 | 36.2837155 | 1.0017155  | 33.015829  |        |
| 0.02137425 | 0.97862575 | 36.2850694 | 1.00171469 | 33.015829  |        |
| 0.02137345 | 0.97862655 | 36.2852818 | 1.00171456 | 33.015829  |        |
| 0.02137333 | 0.97862667 | 36.2853151 | 1.00171454 | 33.015829  |        |
| 0.02137331 | 0.97862669 | 36.2853203 | 1.00171454 | 33.015829  |        |
| 0.0213733  | 0.9786267  | 36.2853211 | 1.00171454 | 33.015829  |        |
| 0.0213733  | 0.9786267  | 36.2853213 | 1.00171454 | 33.015829  |        |
| 0.0213733  | 0.9786267  | 36.2853213 | 1.00171454 | 33.015829  |        |
| 0.0213733  | 0.9786267  | 36.2853213 | 1.00171454 | 33.015829  |        |
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| 0.0213733  | 0.9786267  | 36.2853213 | 1.00171454 | 33.015829  |        |
| 0.0213733  | 0.9786267  | 36.2853213 | 1.00171454 | 33.015829  |        |
| 0.0213733  | 0.9786267  | 36.2853213 | 1.00171454 | 33.015829  |        |